

# Utility-Scale Distribution-Connected PV in Southern California: Modeling and Field Demonstration Results



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**Integrating PV in Distribution  
Grids: Solutions and  
Technologies**

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# NREL/SCE Hi-Pen PV Integration Project



**5 MW Fixed-Tilt Ground-Mount  
System near Porterville, CA**

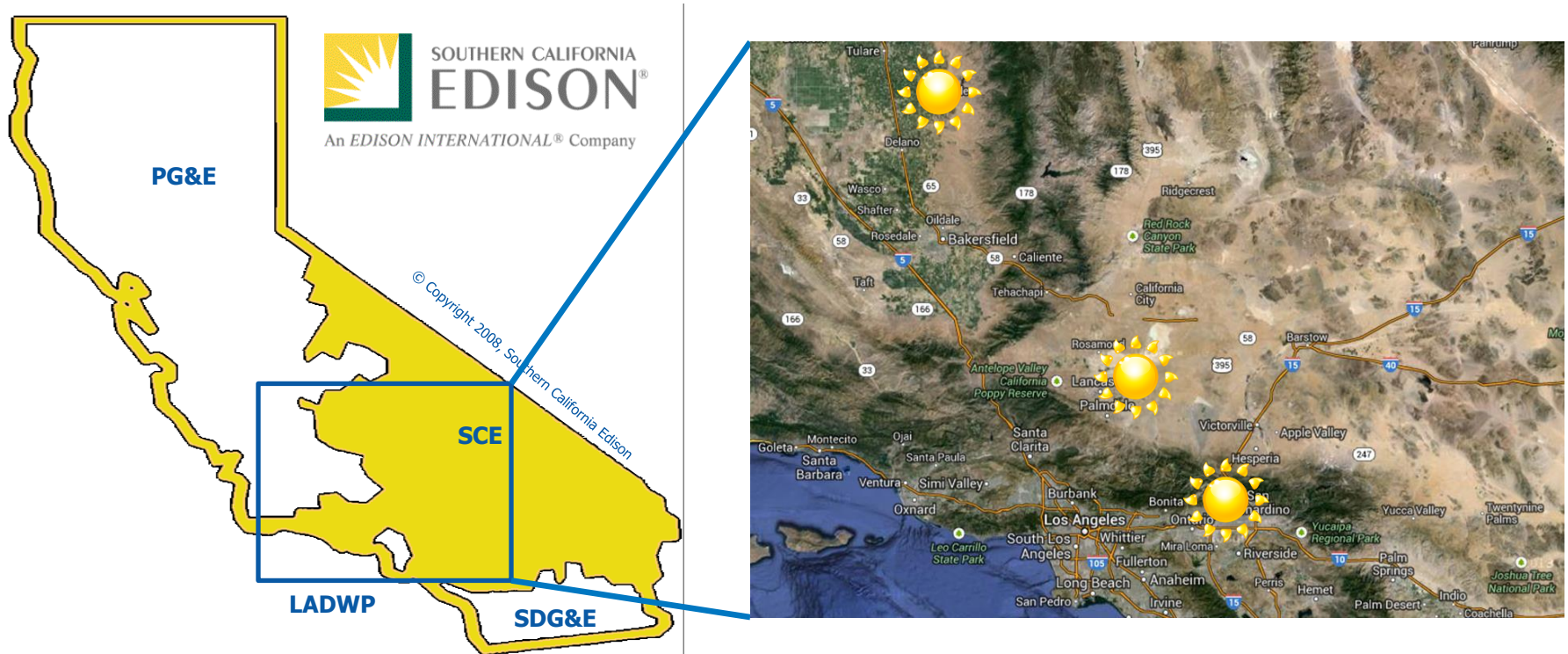


**2 MW Warehouse Roof Mounted  
PV System near Fontana, CA**

- Impetus – in 2009 SCE received approval to install 500 MW of distribution-connected PV in their service territory
- Focus – developing new “rules of thumb” for utility planning engineers for interconnecting large (1-5MW) PV systems on medium voltage (MV) distribution circuits and developing methods to reduce the PV impacts on these systems
- Goal – easing the interconnection concerns of utilities faced with utility-scale distribution-connected PV systems, enabling utility engineers to correctly assess a PV systems potential circuit impacts, and demonstrating that there are current methods for mitigating the impacts of high-penetration PV that can be implemented in the near-term for low cost



# NREL/SCE Study Circuits



## Fontana Characteristics:

- 4.5 MW of PV
- 2 PV systems
- 12 kV
- commercial circuit

## Palmdale Characteristics:

- 3 MW of PV
- 2 PV systems
- 12 kV
- rural circuit
- extremely lightly loaded

## Porterville Characteristics:

- 5 MW of PV
- Single PV system
- 12 kV
- rural circuit
- 40 miles total length

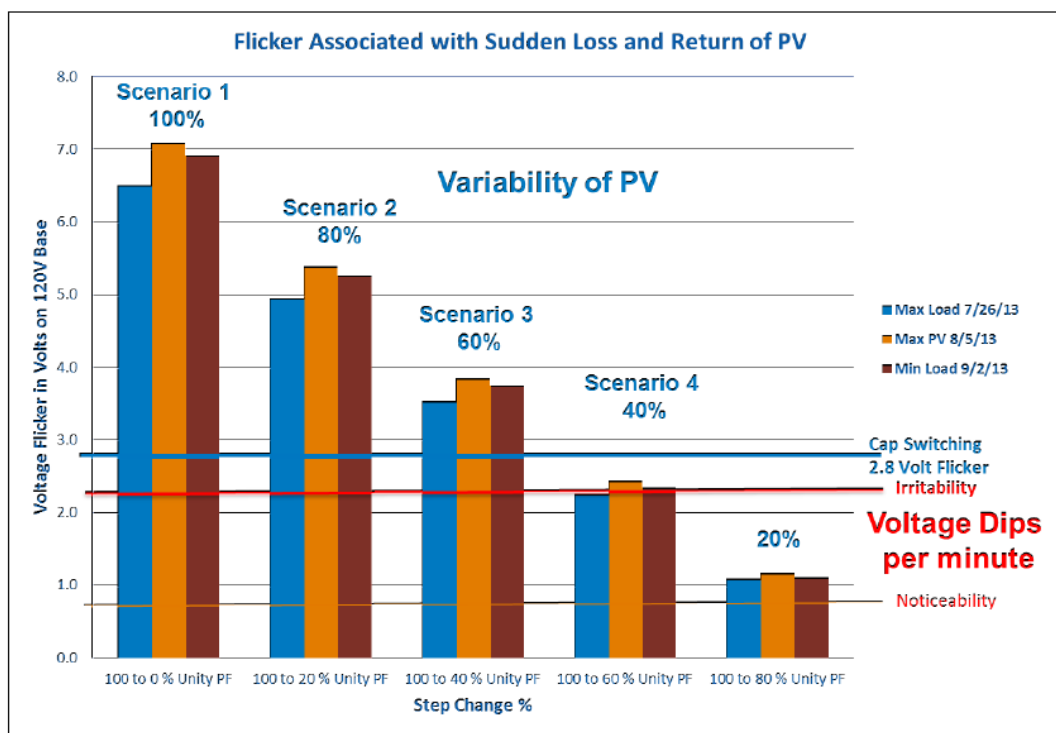


# Dev. of PV Impact Assessment Method

## Developed a PV Impact Methodology Based on Salient Operating Points



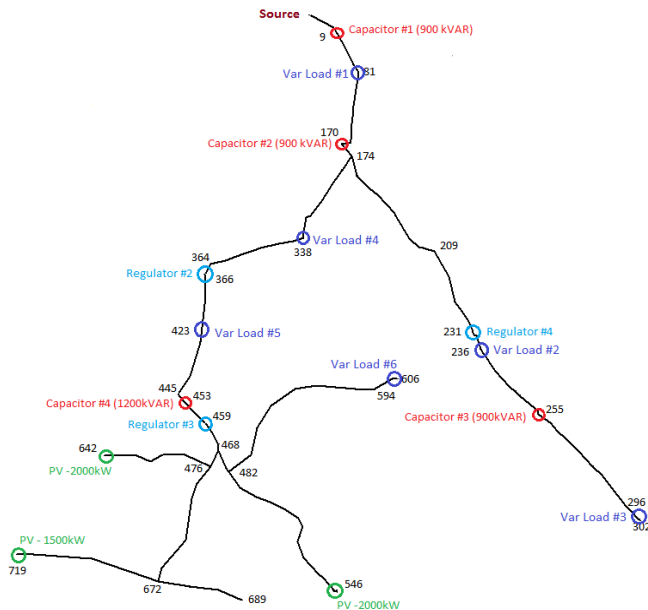
- Investigated PV impact mitigation techniques on the study circuit – utilizing advanced PV inverter functionality
- Assumed worst case PV ramping
- Investigated three loading levels
- Tried to minimize voltage variations below “Noticeability”



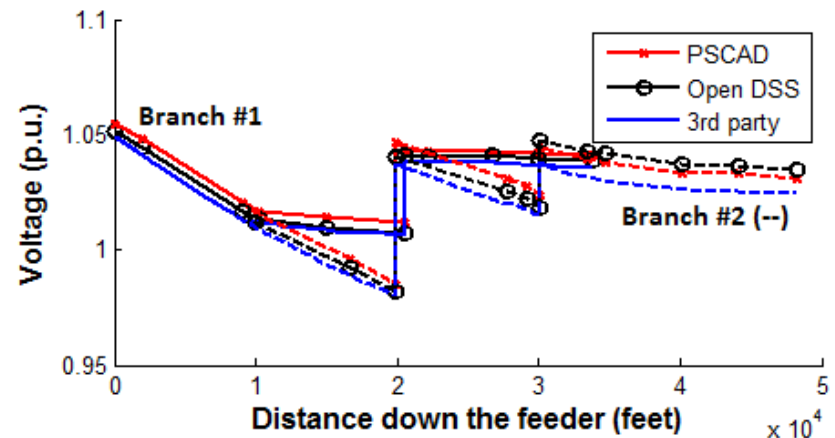
See: B. Mather, et al., “NREL/SCE High Penetration PV Integration Project: FY13 Annual Report,” NREL Tech. Report TP-5D00-61269, June, 2014.

# Comparison of Quasi-Static Time-Series and Transient Simulation Analysis Techniques

## IEEE 8500 node test feeder model



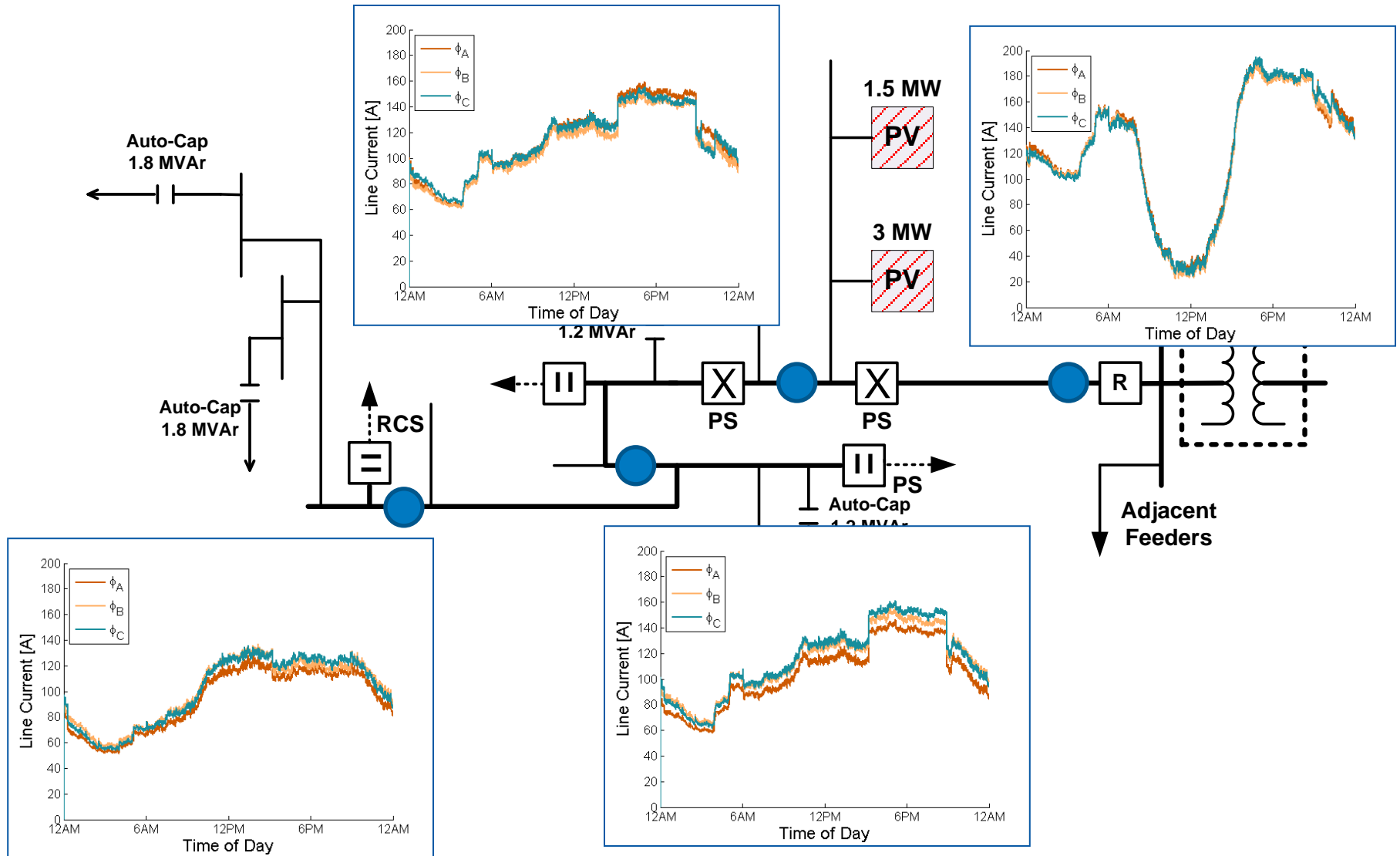
- Evaluated quasi-static time-series analysis results at multiple time steps over a 16 minute period
- Analysis run times are on the order of 5 hours for PSCAD and 5 seconds for OpenDSS



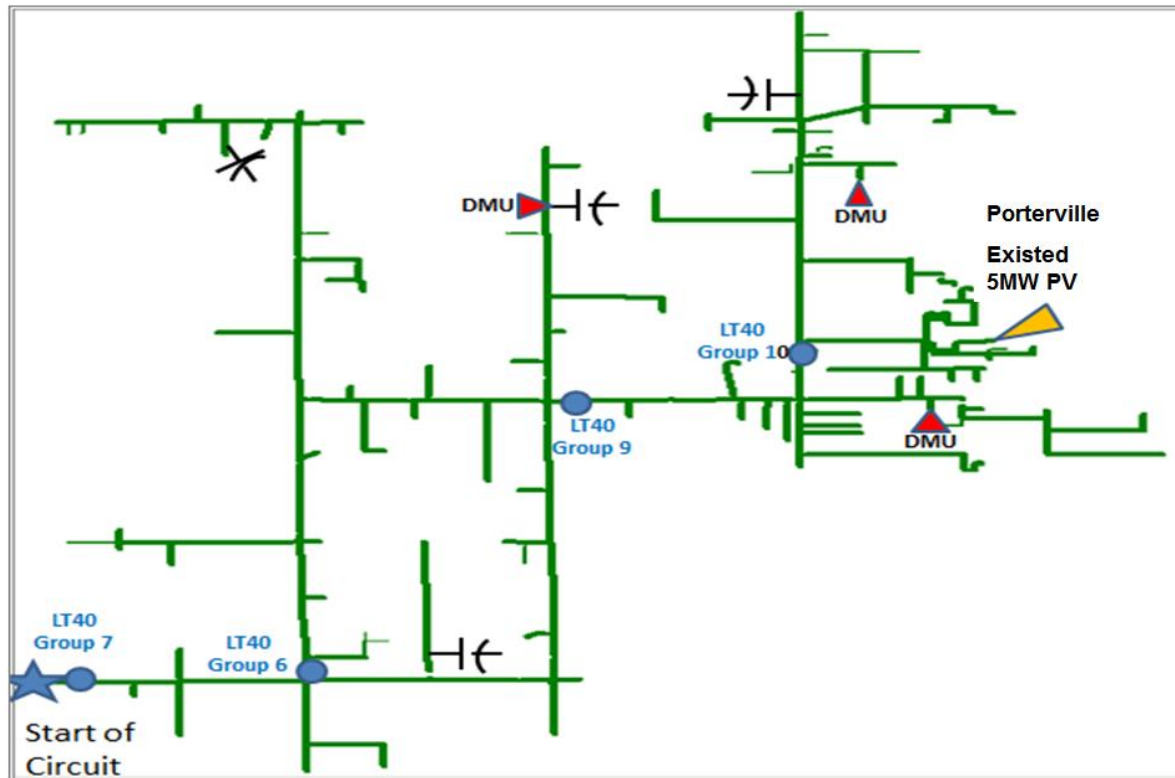
|                  |                  |              | PSCAD        | OpenDSS |     |     |     |     |     |   |
|------------------|------------------|--------------|--------------|---------|-----|-----|-----|-----|-----|---|
|                  |                  |              |              | 5s      | 10s | 15s | 30s | 40s | 50s |   |
| Load tap changer |                  |              | Max          | 5       | 6   | 5   | 5   | 6   | 5   | 5 |
|                  |                  |              | Min          | 4       | 5   | 5   | 5   | 5   | 5   | 5 |
|                  |                  |              | # of actions | 1       | 1   | 0   | 0   | 1   | 0   | 0 |
| Reg. #3          | A                | Max          | 7            | 6       | 6   | 6   | 6   | 6   | 7   |   |
|                  |                  | Min          | 4            | 3       | 3   | 3   | 3   | 4   | 4   |   |
|                  |                  | # of actions | 7            | 6       | 7   | 5   | 8   | 2   | 7   |   |
|                  | B                | Max          | 4            | 4       | 4   | 4   | 4   | 4   | 4   |   |
|                  |                  | Min          | 1            | 2       | 1   | 1   | 1   | 2   | 1   |   |
|                  |                  | # of actions | 8            | 5       | 6   | 5   | 6   | 2   | 7   |   |
|                  | C                | Max          | 2            | 2       | 1   | 1   | 1   | 1   | 1   |   |
|                  |                  | Min          | -1           | -1      | -1  | -1  | -1  | 0   | 0   |   |
|                  |                  | # of actions | 8            | 6       | 6   | 4   | 8   | 1   | 4   |   |
| Cap. #1          | Opening time (s) |              | 489          | 495     | -   | -   | 470 | -   | 150 |   |

See: D. Paradis, F. Katiraei and B. Mather, "Comparative analysis of time-series studies and transient simulations for impact assessment of PV integration on reduces IEEE 8500 node feeder," IEEE PES GM, Vancouver, Canada, July, 2013

# Fontana: Data Acquisition Deployment



# Case Study: Porterville, CA Study Circuit

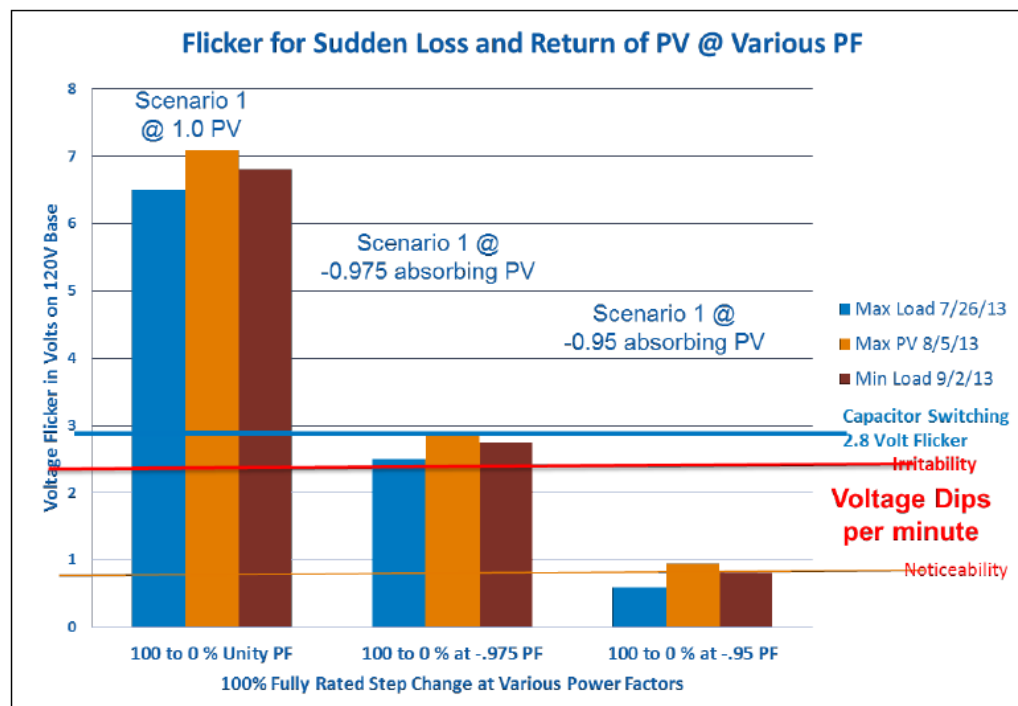


- 5 MW PV fixed-tilt system near the end of the circuit (about 7 miles from the start-of-circuit)
- Circuit is typically lightly loaded (dominated by agricultural pumping load)
- Voltage along the circuit is regulated by switched capacitors

# Determining Mitigation Strategy

## PV Impact Assessment Method – Expanded to Determine PV Mitigation Strategies

- Applied PV Impact Assessment Method (3 salient loading levels)
- Added PV mitigation measures to model and evaluated the effectiveness and “performance” cost of implementing the mitigation measure
- Tried to minimize voltage variations below “Noticeability”

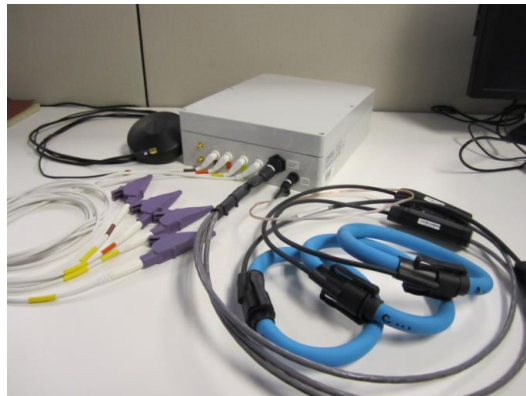


See: B. Mather, et al., “NREL/SCE High Penetration PV Integration Project: FY13 Annual Report,” NREL Tech. Report TP-5D00-61269, June, 2014.

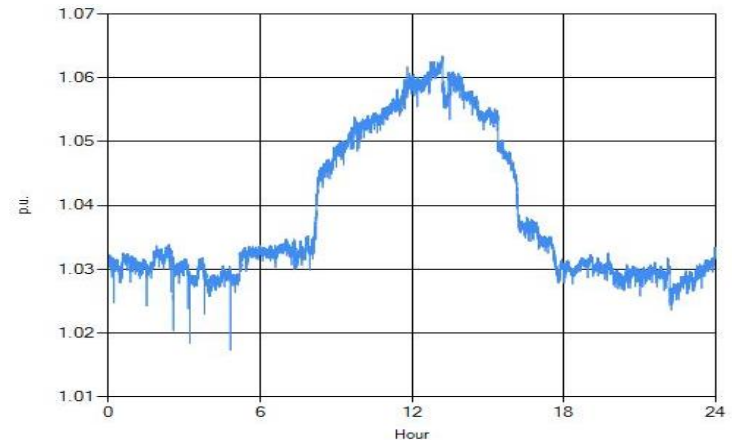


# Field Measurements Show Impact

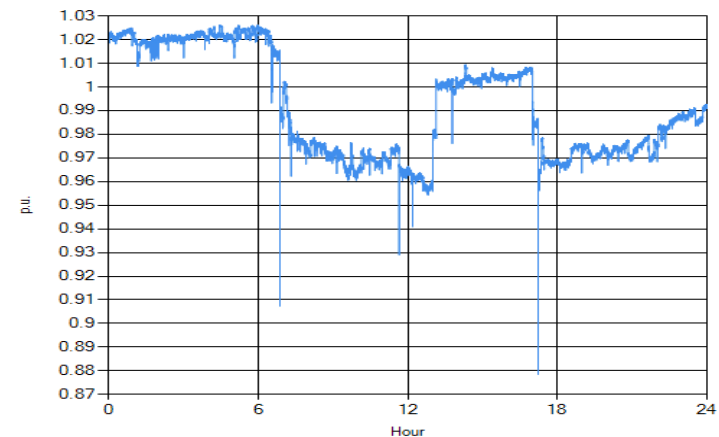
Validated PV assessment method using PV impacts measured on the study circuit



Voltage near PV system – Mostly Sunny Day



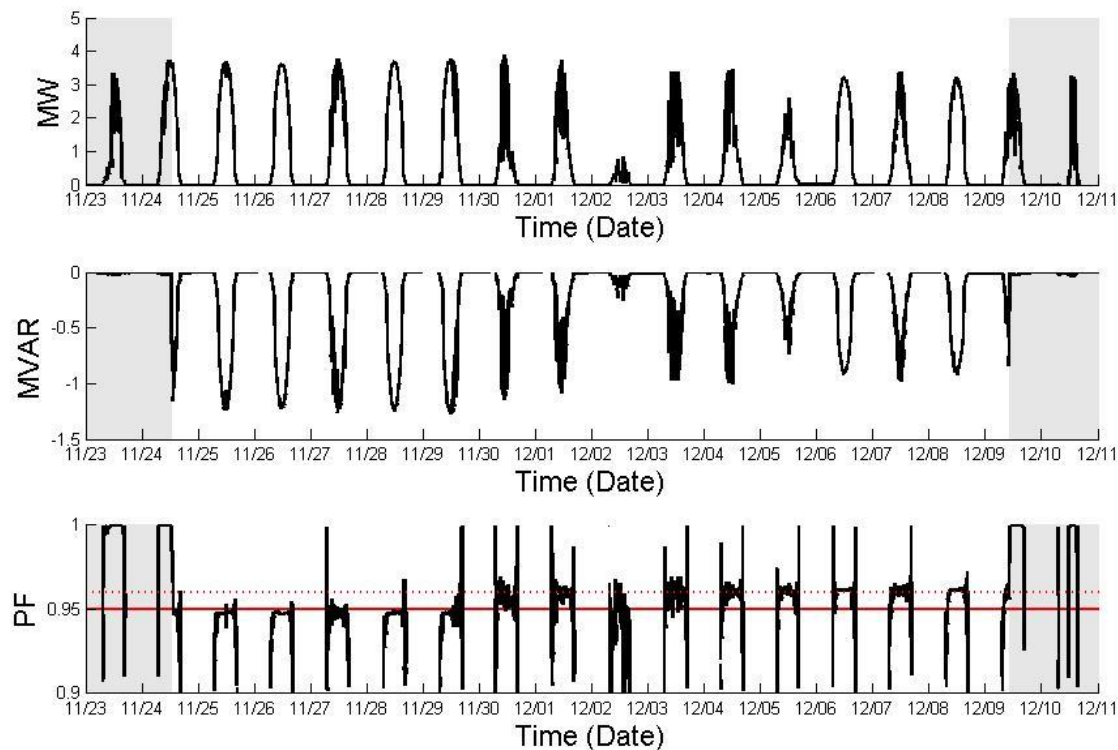
Voltage near PV system – PV Offline



See: F. Katiraei, B. Mather, A. Momeni, L. Yi, and G. Sanchez, "Field Verification and Data Analysis of High Penetration Impacts on Distribution Systems," in proc. of IEEE Photovolt. Spec. Conf., New Orleans, LA, July, 2015



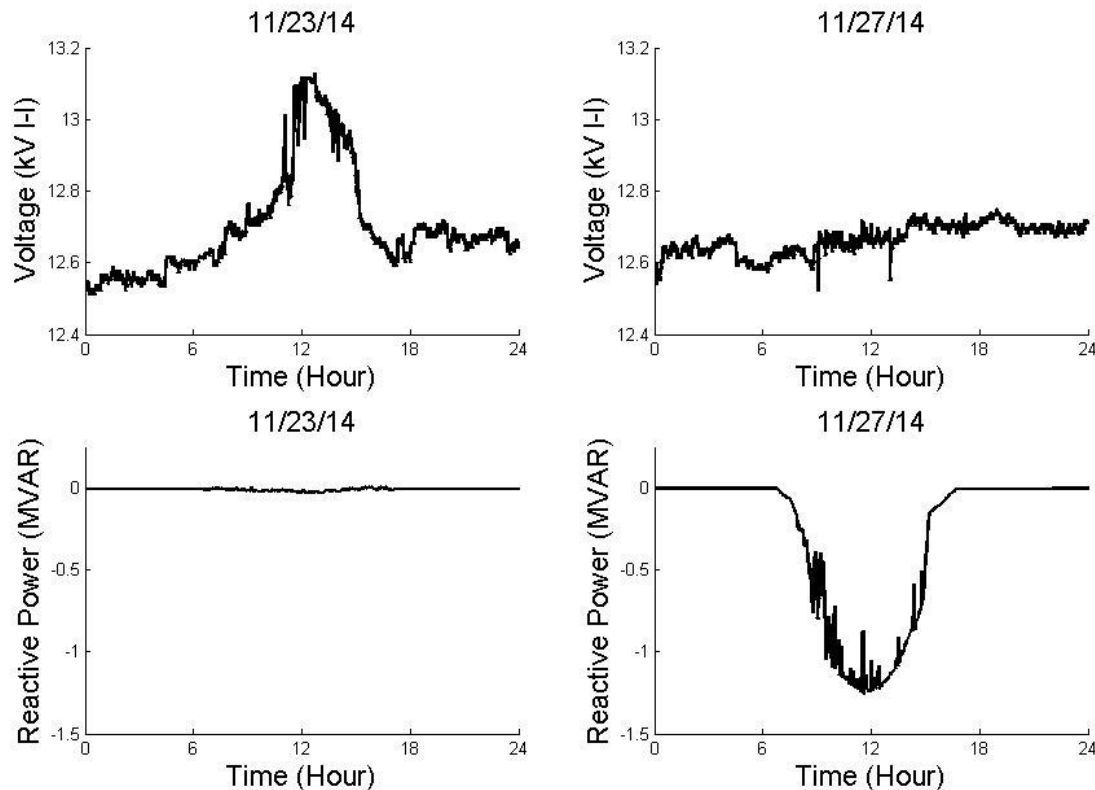
# Demonstration of Adv. Functionality Ability



- All 10 PV inverters were adjusted to operate at an inductive power factor of 0.95.
- On the 5<sup>th</sup> day of the demonstration 2 inverters reverted to unity power factor operation (reasons unclear)

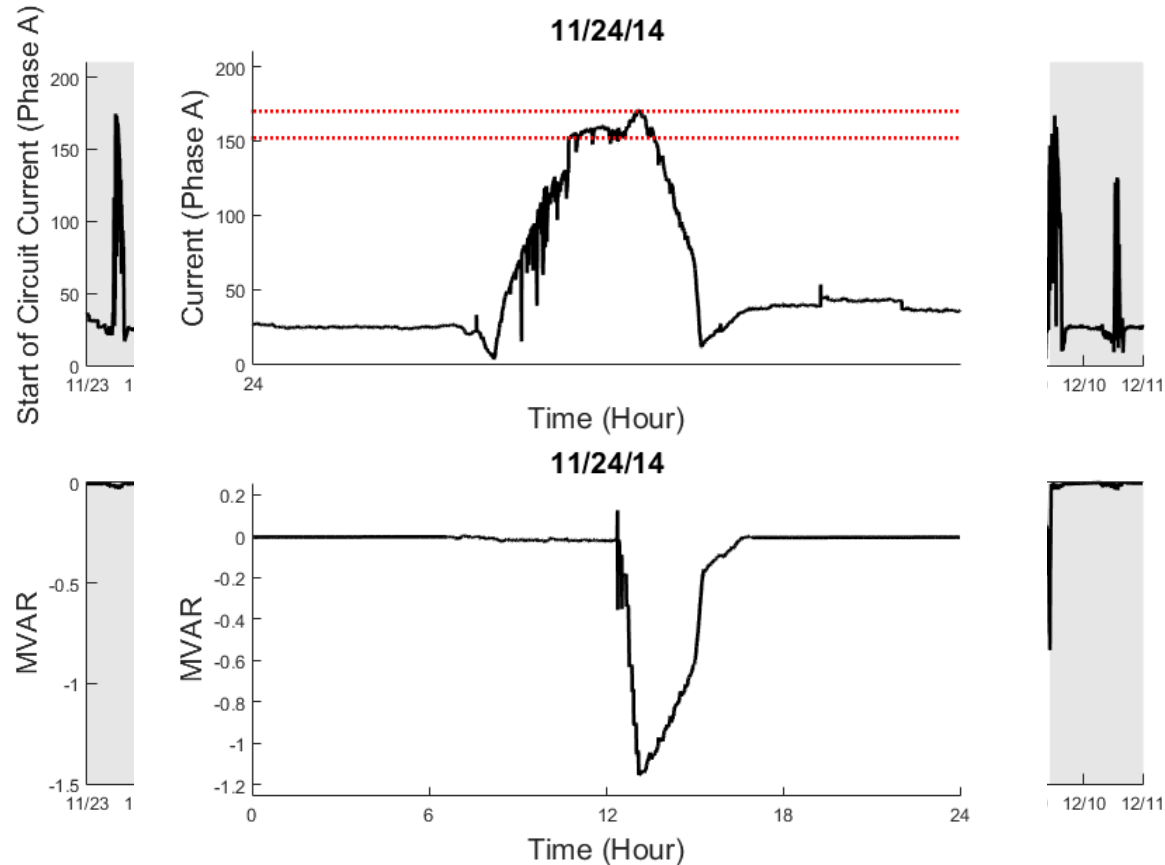
See: B. Mather, A. Gebeheyu, "Field Demonstration of Using Advanced PV Inverter Functionality to Mitigate the Impacts of High-Penetration PV Grid Integration on the Distribution System," in proc. of IEEE Photovolt. Spec. Conf., New Orleans, LA, July, 2015.

# Demonstration of Voltage Impact Mitigation



- During the demonstration period voltage at the PV system's interconnection was less variable.
- Voltage is about 400 V lower or 0.03 per unit.

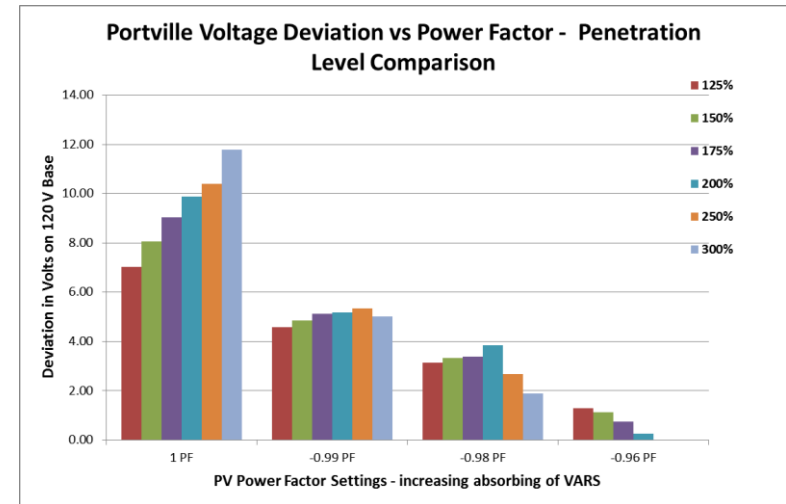
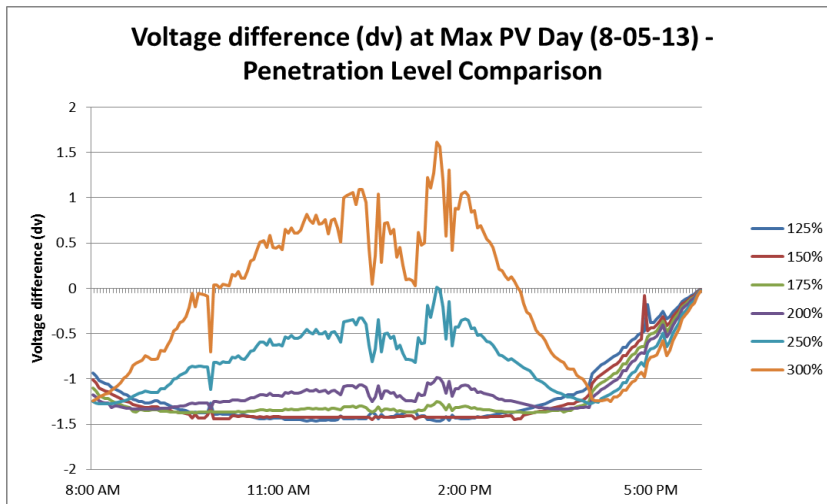
# Impact of Mitigation – Reactive Current



- During the demonstration period current (magnitude) at the start-of-circuit is higher due to reactive current flows.
- Additional current on the circuit is modest.
- Mitigation technique seems compatible with voltage control scheme.
- Allows aggregation of variable reactive current flows at sub-trans./trans. sys,

# Looking forward – What to expect next

This study looked at what distribution-system-level impacts should be expected at even higher rates of PV penetration (up to 300%)



Study findings (generally stated):

- Impact types remain the same – voltage is still dominant impact
- Mitigation becomes more complicated
- 100% loss and return assumptions become increasingly conservative

See: D. Cheng, B. Mather, R. Seguin, J. Hambrick, R. Broadwater, “PV Impact Assessment for Very High Penetration Levels,” in proc. of IEEE Photovolt. Spec. Conf., New Orleans, LA, July, 2015.



# High Penetration PV Integration Handbook



**Developed under the auspices of the NREL/SCE Hi-Pen PV Integration Project Specifically for Distribution Engineers:**

- Condensing the experience gained and research results of the entire project into a handbook for use by distribution engineers facing hi-pen integration challenges in their service territories
- Research expanded to include utility practices and operations beyond just SCE's current practices and operations (i.e. using capacitors as their sole method of voltage regulation)
- Reviewed by practicing distribution engineer experts working on PV interconnection

**Thank you for your attention.**

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